

電子情報通信特論

Advanced Course of Electronics, Information and Communications

Digital Modulation

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自然科学研究科 電気情報工学専攻

Outline

- Signal Space Analysis
- Modulation Schemes
 - Amplitude/Phase Modulation
 - Frequency Modulation
- Pulse Shaping

Digital Modulation

- Benefits
 - Higher spectral efficiency
 - Powerful error correction
 - Resistance to channel impairments
- Linear type: Amplitude and phase modulation
 - 👍 Better spectral efficiency
 - 👎 Not robust against channel impairments
 - 👎 Needs linear amplifiers (expensive and low power efficiency)
- Nonlinear type: Frequency modulation
 - 👎 Worse spectral efficiency
 - 👍 Robust against channel impairments
 - 👍 Nonlinear amplifier is enough (cheap and high power efficiency)

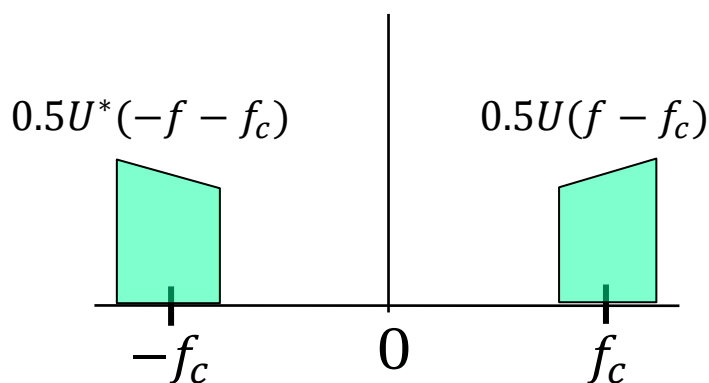
Modulated Signal Representation

- Bandpass signal (passband; real signal)

$$s(t) = A(t) \cos(2\pi f_c t + \theta(t)) = \text{Re}[e^{j2\pi f_c t} A(t) e^{j\theta(t)}]$$

- Lowpass signal (baseband; complex signal)

$$u(t) = A(t)e^{j\theta(t)} = A(t)(\cos\theta(t) + j \sin\theta(t))$$

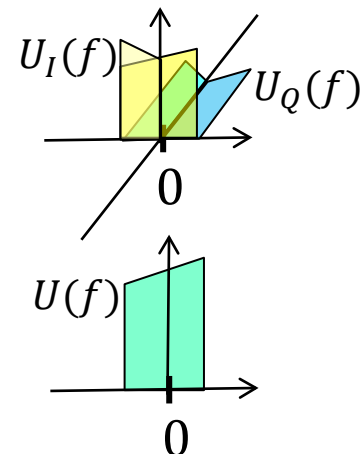
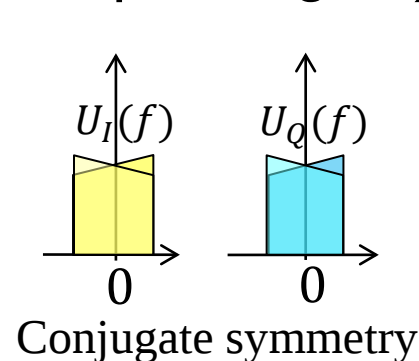


$$\begin{aligned} s(t) &= \text{Re}[u(t)e^{j2\pi f_c t}] \\ &= u_I(t) \cos 2\pi f_c t - u_Q(t) \sin 2\pi f_c t \\ &= \frac{1}{2} (u(t)e^{j2\pi f_c t} + u^*(t)e^{-j2\pi f_c t}) \\ \mathcal{F}\{s(t)\} &= \frac{1}{2} (U(f - f_c) + U^*(-f - f_c)) \end{aligned}$$

Quadrature Modulation

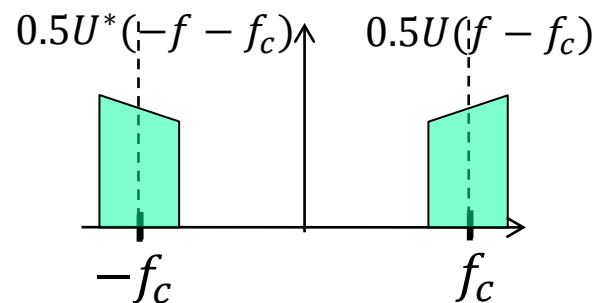
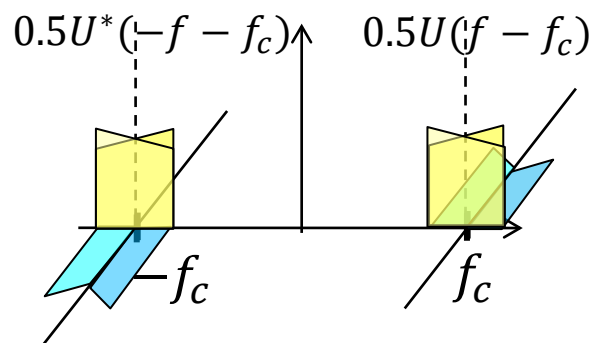
- Lowpass signal (baseband; complex signal)

$$\begin{aligned}
 & \mathcal{F} \left\{ \begin{aligned} & u(t) = u_I(t) + j u_Q(t) \\ & U(f) = U_I(f) + j U_Q(f) \\ & U^*(-f) = U_I(f) - j U_Q(f) \\ & U_I(f) = 0.5[U(f) + U^*(-f)] \\ & U_Q(f) = 0.5/j[U(f) - U^*(-f)] \end{aligned} \right.
 \end{aligned}$$



- Q-Mod and bandpass signal generation

$$\mathcal{F}\{\text{Re}[u(t)e^{j2\pi f_c t}]\} = 0.5(U(f - f_c) + U^*(-f - f_c))$$



Quadrature Demodulation

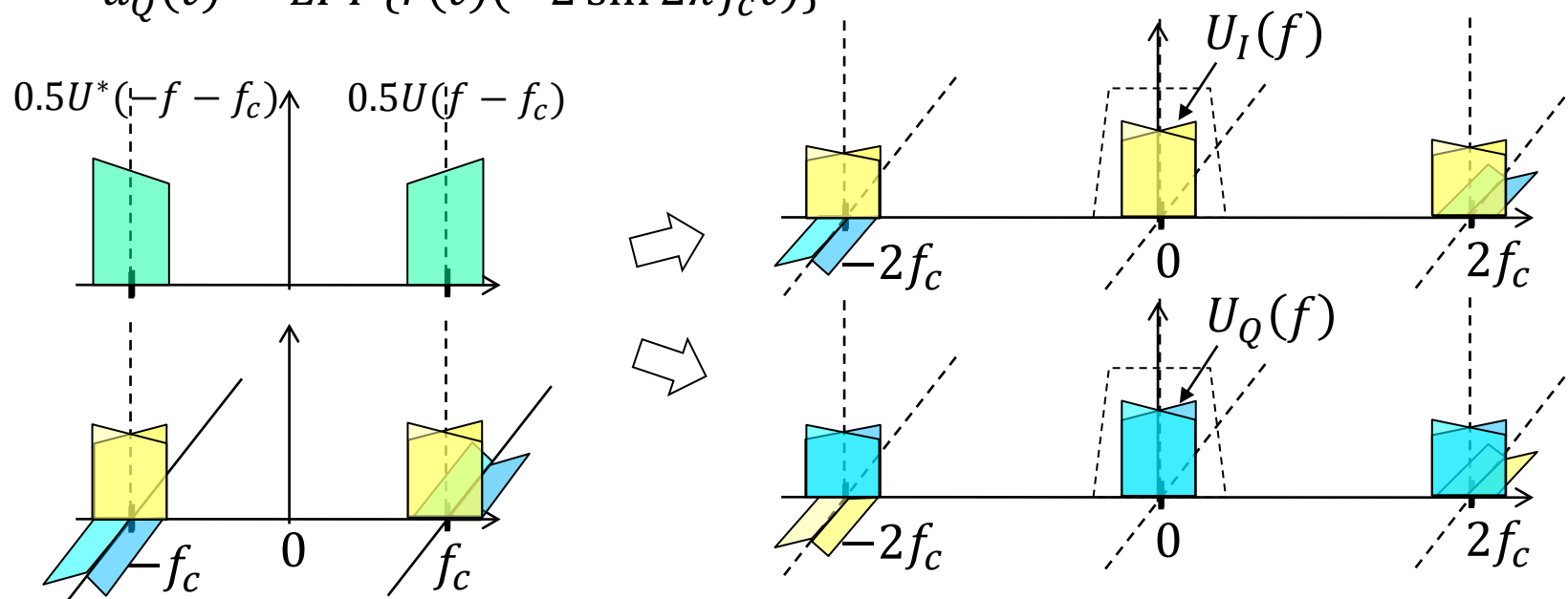
- Bandpass signal

$$\begin{aligned} r(t) &= \text{Re}[u(t)e^{j2\pi f_c t}] = u_I(t) \cos 2\pi f_c t - u_Q(t) \sin 2\pi f_c t \\ &= \frac{1}{2} (u(t)e^{j2\pi f_c t} + u^*(t)e^{-j2\pi f_c t}) \end{aligned}$$

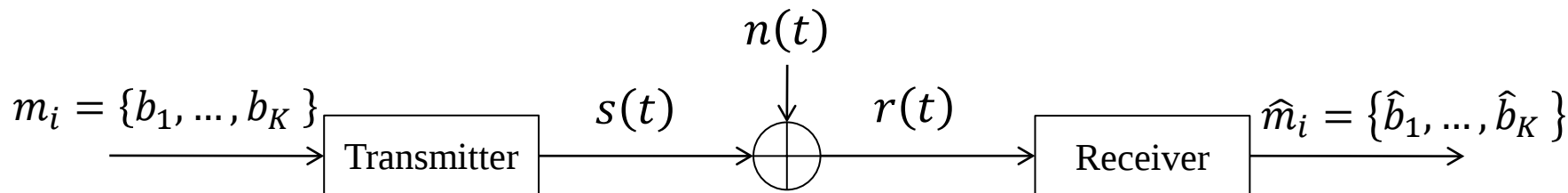
- Q-demod and lowpass signal extraction

$$u_I(t) = \text{LPF}\{r(t)(2 \cos 2\pi f_c t)\}$$

$$u_Q(t) = \text{LPF}\{r(t)(-2 \sin 2\pi f_c t)\}$$



System Model (AWGN)

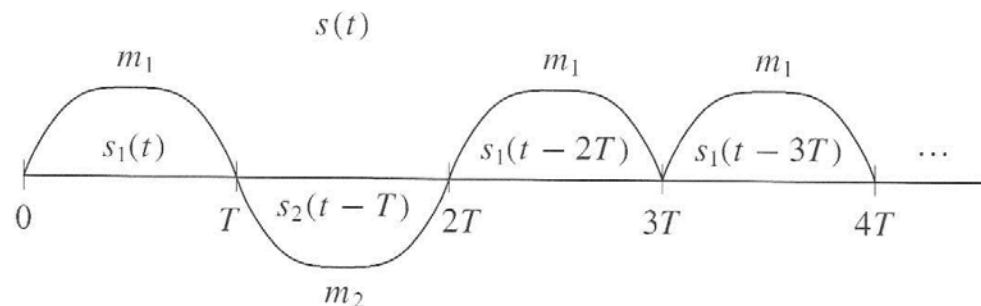


- Symbol period: T seconds
- Data per unit time: $K = \log_2 M$ [bits]
- Data rate: $R = \frac{K}{T}$ [bps]
- There are $M = 2^K$ possible sequences of K bits
 - A message $m_i = \{b_1, \dots, b_K\} \in \mathcal{M}$ is comprised of a bit sequence of length K where $\mathcal{M} = \{m_1, \dots, m_M\}$
 - The messages have probability p_i of being selected for transmission, where $\sum p_i = 1$

System Model (AWGN)

- Suppose message m_i is to be transmitted over the channel during time interval $[0, T)$
- Each message $m_i \in \mathcal{M}$ is mapped to a unique signal $s_i \in S$ where $S = \{s_1(t), \dots, s_M(t)\}$
- Energy

$$E_{s_i} = \int_0^T s_i^2(t) dt, \quad i = 1, \dots, M$$



- Detection

$$P_e = \sum_{i=1}^M p(\hat{m} \neq m_i | m_i \text{ sent}) p(m_i \text{ sent})$$

Geometrical Representation

- Any set of M real signals defined on $[0, T)$ with finite energy can be represented as a linear combination of $N \leq M$ real orthonormal basis functions $\{\phi_1(t), \dots, \phi_N(t)\}$ as

$$s_i(t) = \sum_{j=1}^N s_{ij} \phi_j(t)$$

Gram-Schmidt
Orthogonalization procedure

where the coefficient, $s_{ij} = \int_0^T s_i(t) \phi_j(t) dt$

- Basis functions span the set S and

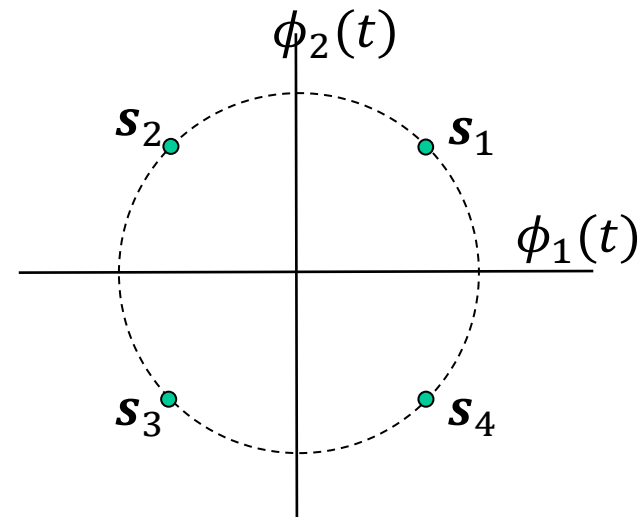
$$\int_0^T \phi_i(t) \phi_j(t) dt = \begin{cases} 1 & i = j \\ 0 & i \neq j \end{cases}$$

Signal Space

- Minimum number $N \simeq 2BT$ ($s_i(t)$ occupies $2BT$ orthogonal dimension)
- Linear passband modulation

$$\phi_1(t) = \sqrt{\frac{2}{T}} \cos 2\pi f_c t, \quad \phi_2(t) = \sqrt{\frac{2}{T}} \sin 2\pi f_c t$$

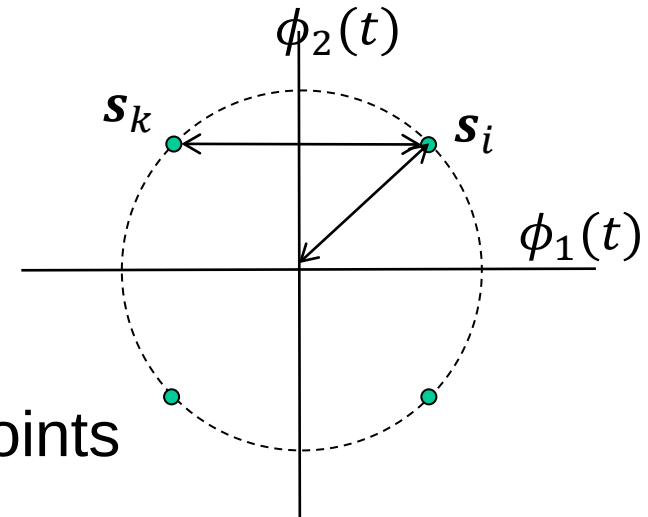
- Signal constellation
 - $\mathbf{s}_i = [s_{i1}, \dots, s_{iN}]^T \in \mathbb{R}^N$
 - $s_i(t)$ is represented by $\mathbf{s}_i$
(signal space representation)
 - MPSK and MQAM
→ 2-dim (in-phase and quadrature)



Signal Space Representation

- Length of the vector

$$\|\mathbf{s}_i\| \triangleq \sqrt{\sum_{j=1}^N s_{ij}^2}$$



- Distance between two constellation points

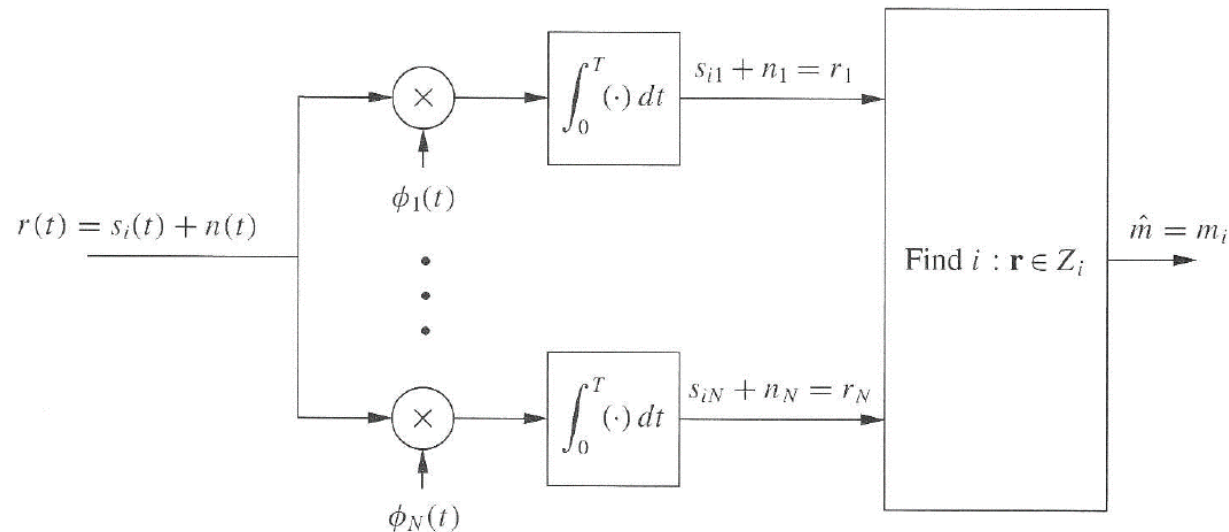
$$\|\mathbf{s}_i - \mathbf{s}_k\| = \sqrt{\sum_{j=1}^N (s_{ij} - s_{kj})^2} = \sqrt{\int_0^T (s_i(t) - s_k(t))^2 dt}$$

- Inner product

$$\langle \mathbf{s}_i, \mathbf{s}_k \rangle = \mathbf{s}_i^T \mathbf{s}_k = \int_0^T s_i(t) s_k(t) dt = \langle s_i(t), s_k(t) \rangle$$

Receiver Structure

- Receiver structure for signal detection in AWGN



$$r(t) = \sum_{j=1}^N (s_{ij} + n_j) \phi_j(t) + n_r(t) = \sum_{j=1}^N r_j \phi_j(t) + n_r(t)$$

$$s_{ij} = \int_0^T s_i(t) \phi_j(t) dt, \quad n_j = \int_0^T n(t) \phi_j(t) dt, \quad n_r(t) = n(t) - \sum_{j=1}^N n_j \phi_j(t)$$

$\mathbf{r} = [r_1, \dots, r_N]$ is sufficient statistics for $r(t)$ in the optimum detection

Decision Regions and MLD

- The optimum receiver minimizes error prob. by selecting the detector output $\hat{m} \rightarrow$ maximizes $1 - P_e = p(\hat{m} \text{ sent} | \mathbf{r})$
- Decision region

$$Z_i = \{\mathbf{r}: p(\mathbf{s}_i \text{ sent} | \mathbf{r}) > p(\mathbf{s}_j \text{ sent} | \mathbf{r}) \forall j \neq i\}$$

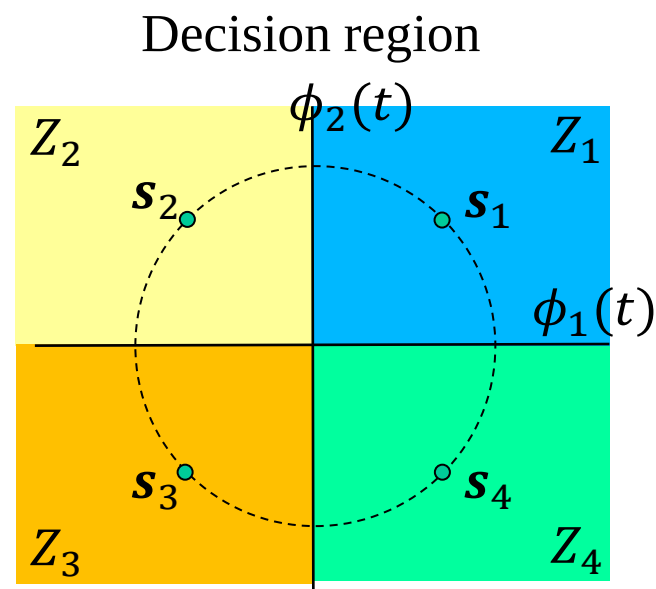
- Bayes' rule

$$p(\mathbf{s}_i | \mathbf{r}) = \frac{p(\mathbf{r} | \mathbf{s}_i) p(\mathbf{s}_i)}{p(\mathbf{r})}$$

- Maximum likelihood detection

$$\arg \max_{\mathbf{s}_i} p(\mathbf{s}_i | \mathbf{r}) \leftrightarrow \arg \max_{\mathbf{s}_i} p(\mathbf{r} | \mathbf{s}_i)$$

$$L(\mathbf{s}_i) = p(\mathbf{r} | \mathbf{s}_i) \quad \text{likelihood function}$$



Maximum Likelihood Receiver

- Conditioned distribution of $\mathbf{r}$

$$p(\mathbf{r}|\mathbf{s}_i) = \prod_{j=1}^N p(r_j|m_i) = \frac{1}{(\pi N_0)^{N/2}} \exp \left[-\frac{1}{N_0} \sum_{j=1}^N (r_i - s_{ij})^2 \right]$$

where r_i is a Gauss-distributed RV that is independent of r_k ($k \neq j$)
with mean s_{ij} and variance $\frac{N_0}{2}$

- Log likelihood function

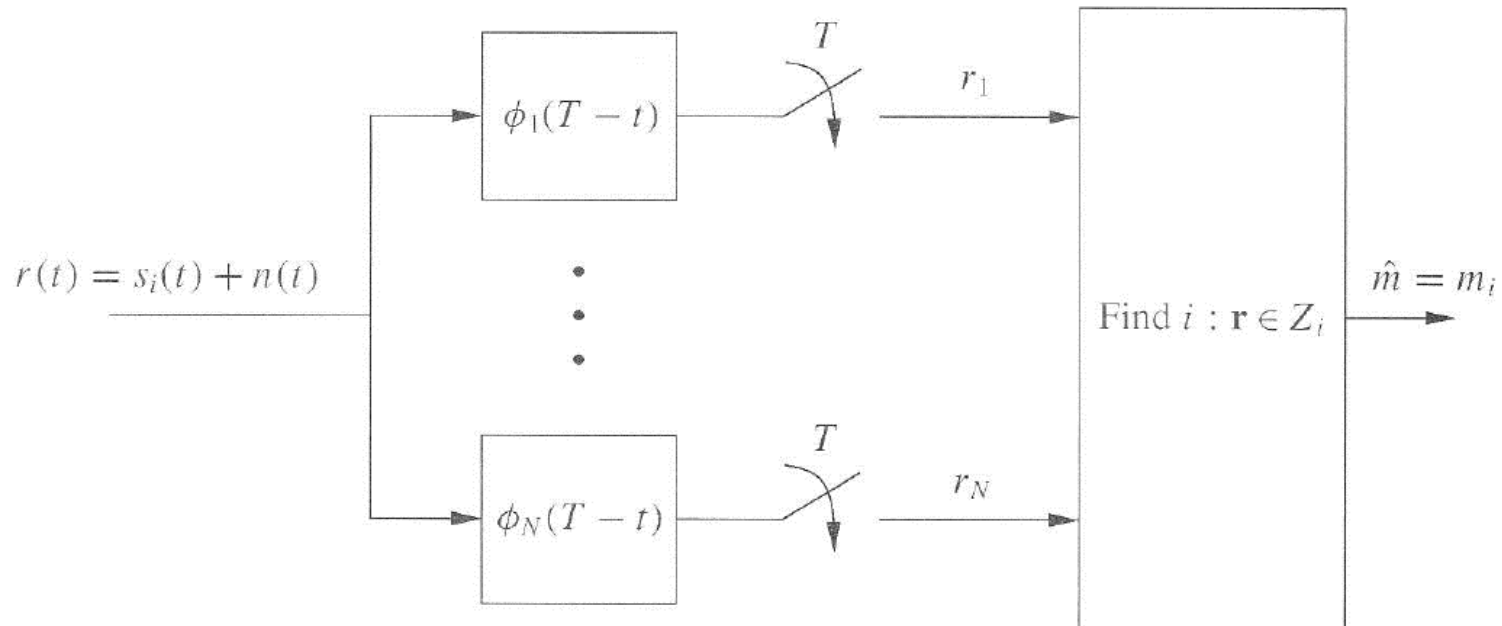
$$l(\mathbf{s}_i) = -\frac{1}{N_0} \sum_{j=1}^N (r_i - s_{ij})^2 = -\frac{1}{N_0} \|\mathbf{r} - \mathbf{s}_i\|^2$$

- ML receiver

$$\arg \min_{\mathbf{s}_i} \|\mathbf{r} - \mathbf{s}_i\|^2$$

Matched Filter Receiver

- Matched filter receiver structure



$$y_j(t) = \int_0^t r(\tau) h_j(t - \tau) d\tau = \int_0^t r(\tau) \phi_j(T - t + \tau) d\tau$$

$$r_j = y_j(T) = \int_0^T r(\tau) \phi_j(\tau) d\tau \quad \text{equivalent to correlation detector}$$

Error Probability

- For equally likely messages, the error probability

$$\begin{aligned}
 P_e &= \sum_{i=1}^M p(\mathbf{r} \notin Z_i | m_i \text{ sent}) p(m_i \text{ sent}) \\
 &= 1 - \frac{1}{M} \sum_{i=1}^M p(\mathbf{r} \in Z_i | m_i \text{ sent}) = 1 - \frac{1}{M} \sum_{i=1}^M \int_{Z_i} p(\mathbf{r} | m_i) d\mathbf{r} \\
 &= 1 - \frac{1}{M} \sum_{i=1}^M \int_{Z_i} p(\mathbf{r} = \mathbf{s}_i + \mathbf{n} | \mathbf{s}_i) d\mathbf{n} = 1 - \frac{1}{M} \sum_{i=1}^M \int_{Z_i - \mathbf{s}_i} p(\mathbf{n}) d\mathbf{n}
 \end{aligned}$$

- Error probability conditioned that m_i is sent

$$P_e(m_i \text{ sent}) = p\left(\bigcup_{\substack{k=1 \\ k \neq i}}^M A_{ik}\right) \leq \sum_{\substack{k=1 \\ k \neq i}}^M p(A_{ik})$$

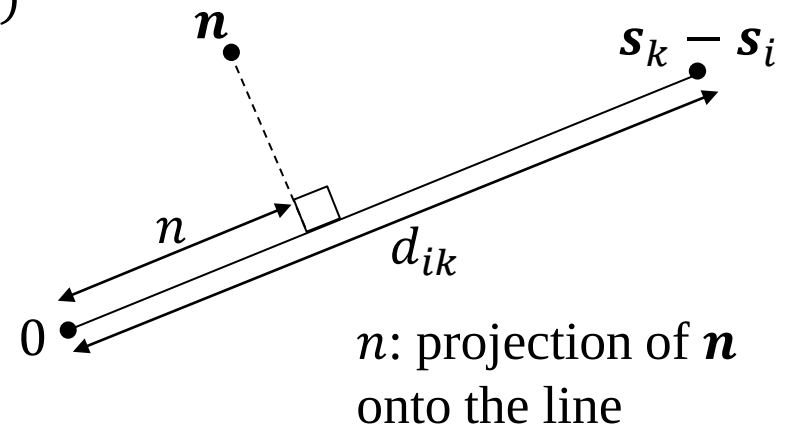
where A_{ik} denotes the event that $\|\mathbf{r} - \mathbf{s}_k\| < \|\mathbf{r} - \mathbf{s}_i\|$

Error Probability

■ Prob. event A_{ik}

$$\begin{aligned} p(A_{ik}) &= p(\|\mathbf{s}_k - \mathbf{r}\| < \|\mathbf{s}_i - \mathbf{r}\| | \mathbf{s}_i \text{ sent}) \\ &= p(\|\mathbf{s}_k - \mathbf{s}_i - \mathbf{n}\| < \|\mathbf{n}\|) \end{aligned}$$

$$\begin{aligned} p(A_{ik}) &= p\left(n > \frac{d_{ik}}{2}\right) \\ &= \int_{\frac{d_{ik}}{2}}^{\infty} \frac{1}{\sqrt{\pi N_0}} \exp\left[-\frac{v^2}{N_0}\right] dv = Q\left(\frac{d_{ik}}{\sqrt{2N_0}}\right) \end{aligned}$$



■ Prob. error

$$P_e(m_i \text{ sent}) \leq \sum_{\substack{k=1 \\ k \neq i}}^M Q\left(\frac{d_{ik}}{\sqrt{2N_0}}\right)$$

$$P_e = \sum_{i=1}^M P_e(m_i \text{ sent}) p(m_i \text{ sent}) \leq \frac{1}{M} \sum_{i=1}^M \sum_{\substack{k=1 \\ k \neq i}}^M Q\left(\frac{d_{ik}}{\sqrt{2N_0}}\right)$$

Nearest Neighbor Approximation

- Introducing the minimum distance of the constellation as $d_{\min} = \min_{i,k} d_{ik}$, we can simplify with the looser bound

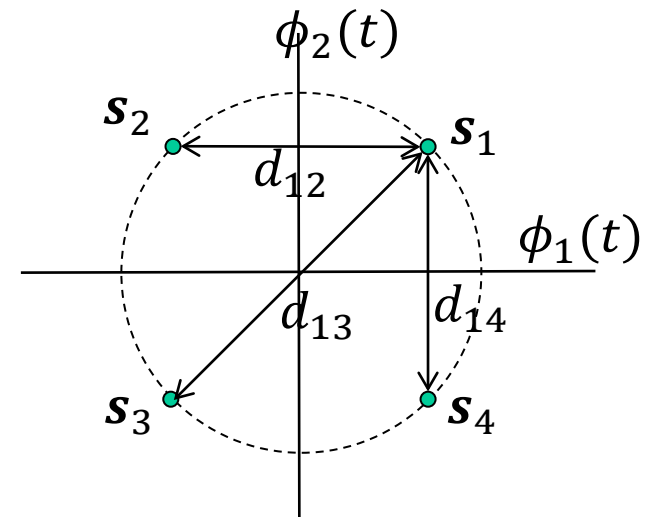
$$P_e \leq (M - 1)Q\left(\frac{d_{\min}}{\sqrt{2N_0}}\right)$$

- Nearest neighbor approximation

$$P_e \approx M_{d_{\min}} Q\left(\frac{d_{\min}}{\sqrt{2N_0}}\right)$$

$M_{d_{\min}}$: the number of neighbors at $d_{\min}$

- For BPSK, $M = 2$, and $M_{d_{\min}} = 1 \rightarrow P_b = Q\left(\frac{d_{\min}}{\sqrt{2N_0}}\right)$
- By mapping gray code, $P_b \approx \frac{P_e}{\log_2 M}$



Various Modulation Schemes

- Bandpass signal

$$s(t) = A(t) \cos(2\pi f_c t + \theta(t)) = \text{Re}[u(t)e^{j2\pi f_c t}]$$

- Lowpass signal

$$u(t) = s_I(t) + js_Q(t) = A(t)e^{j\theta(t)}$$

The diagram illustrates the decomposition of the lowpass signal $u(t) = A(t)e^{j\theta(t)}$ into three modulation schemes:

- Amplitude Modulation (MPAM)**: Derived from the amplitude term $A(t)$.
- Phase Modulation (MPSK)**: Derived from the phase term $\theta(t)$.
- Frequency Modulation (FSK, MSK)**: Derived from the frequency term $\frac{1}{2\pi} \frac{d\theta(t)}{dt}$.

A bracket under Amplitude Modulation (MPAM) and Phase Modulation (MPSK) indicates they are combined as **Amplitude & Phase Modulation (MQAM)**.

Amplitude and Phase Modulation

- Bandpass signal

$$s(t) = s_I(t) \cos 2\pi f_c t - s_Q(t) \sin 2\pi f_c t$$

- Signal space representation

$$s(t) = s_{i1}\phi_1(t) + s_{i2}\phi_2(t) \quad i = 1, \dots, M$$

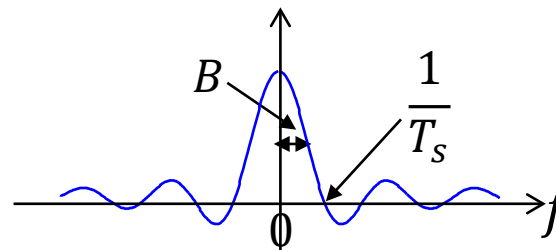
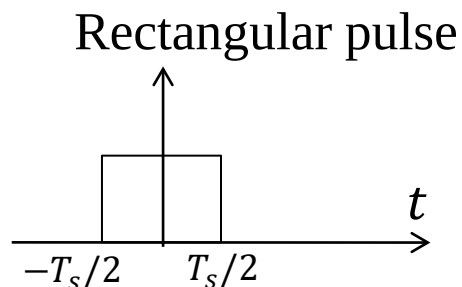
Base functions

$$\begin{aligned} \phi_1(t) &= g(t) \cos(2\pi f_c t + \varphi_0) \\ \phi_2(t) &= -g(t) \sin(2\pi f_c t + \varphi_0) \end{aligned}$$

Baseband signals

$$\begin{aligned} s_I(t) &= s_{i1}g(t) \\ s_Q(t) &= s_{i2}g(t) \end{aligned}$$

- Pulse shape $g(t)$ is a signal with bandwidth of B

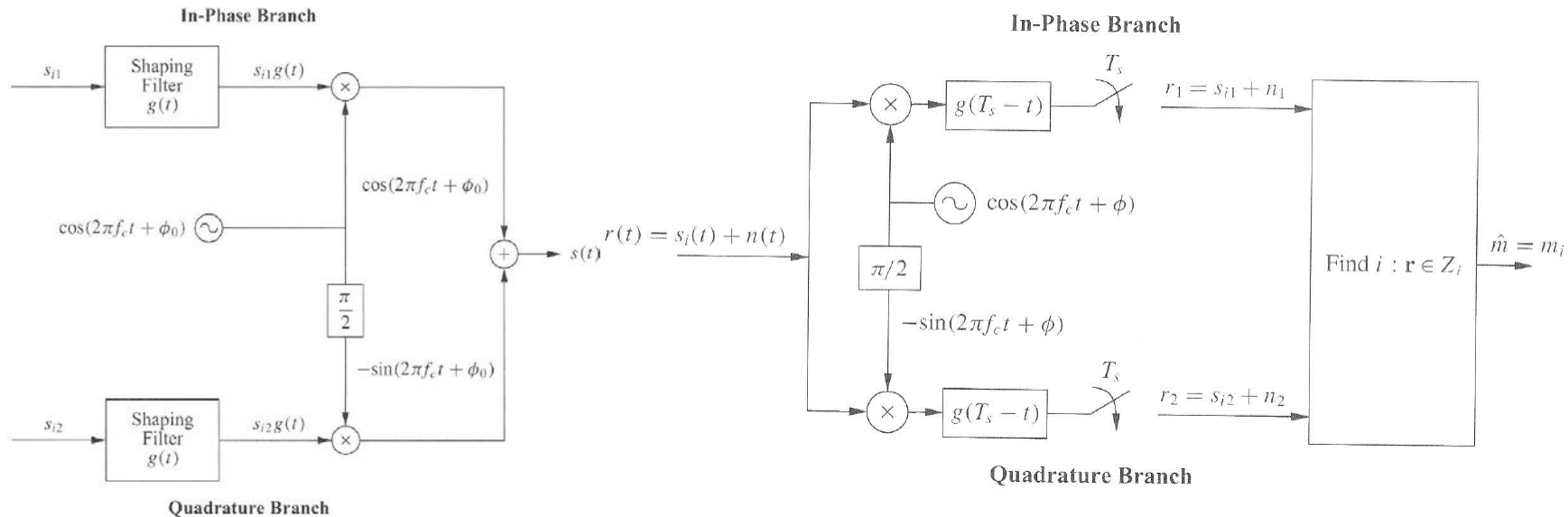


$$T_s = \frac{1}{2B}$$

Nyquist rate

Amplitude and Phase Modulation

■ Amplitude and phase modulation / demodulation



- **Carrier phase recovery:** to match carrier phases (ϕ_0 and ϕ)
 → *Coherent detection*
- **Synchronization or timing recovery:** to find the start of the symbol period

Pulse Amplitude Modulation (MPAM)

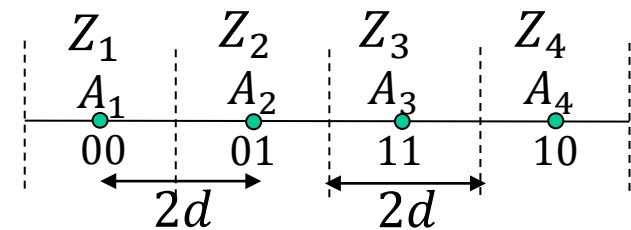
■ Modulated signal

$$s_i(t) = \text{Re}[A_i g(t) e^{j2\pi f_c t}] = A_i g(t) \cos 2\pi f_c t \quad 0 \leq t \leq T_s \gg 1/f_c$$

$$A_i = (2i - 1 - M)d, \quad i = 1, \dots, M$$

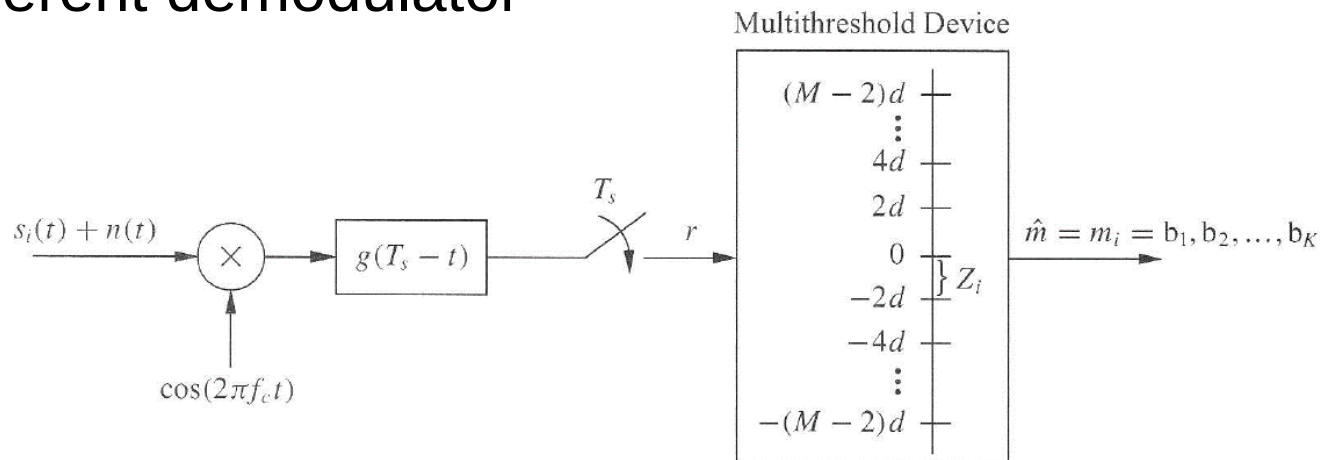
$$d_{\min} = 2d$$

$$E_{s_i} = \int_0^{T_s} s_i^2(t) dt = A_i^2 \quad E_s = \frac{1}{M} \sum_{i=1}^M A_i^2$$



<4PAM($M = 4, K = 2$)>

■ Coherent demodulator



Phase Shift Keying (MPSK)

- Modulated signal over one symbol time T_s $0 \leq t \leq T_s$

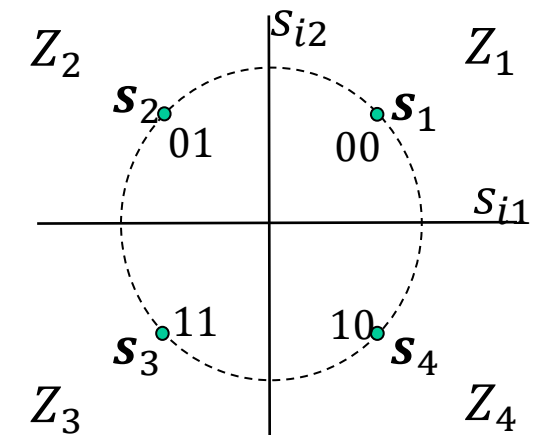
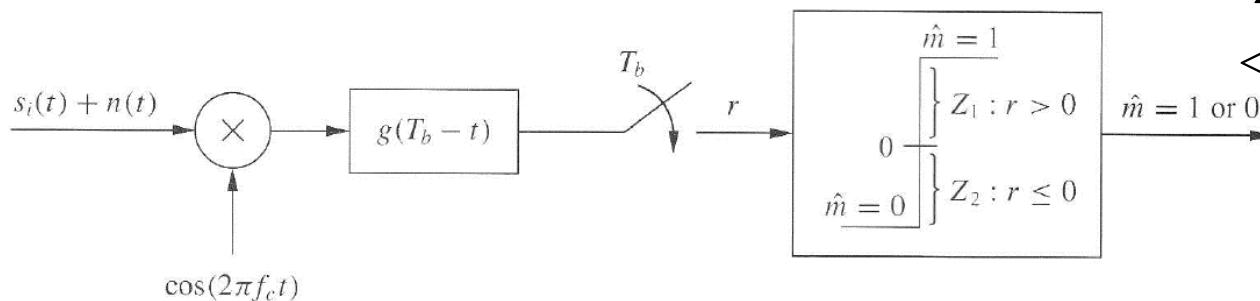
$$s_i(t) = \text{Re} \left[A e^{j \left(2\pi \frac{(i-1)}{M} + \frac{\pi}{4} \right)} g(t) e^{j 2\pi f_c t} \right] = A g(t) \cos \left(2\pi f_c t + 2\pi \frac{(i-1)}{M} + \frac{\pi}{4} \right)$$

$$s_{i1}(t) = A \cos \left(2\pi \frac{(i-1)}{M} + \frac{\pi}{4} \right), \quad s_{i2}(t) = A \sin \left(2\pi \frac{(i-1)}{M} + \frac{\pi}{4} \right)$$

$$d_{\min} = 2A \sin \left(\frac{\pi}{M} \right)$$

$$E_{s_i} = \int_0^{T_s} s_i^2(t) dt = A^2 \quad (\text{Equal energy})$$

- Coherent demodulator for BPSK



$\langle \text{QPSK}(M = 4, K = 2) \rangle$

Quadrature Amplitude Modulation (MQAM)

- Modulated signal over one symbol time T_s

$$s_i(t) = \text{Re}[A_i e^{j\theta_i} g(t) e^{j2\pi f_c t}] = A_i g(t) \cos(2\pi f_c t + \theta_i)$$

s_{i1} , and s_{i2} take values on $(2i - 1 - L)d$ for $i = 1, \dots, L$

→ 2-D extension of MPAM

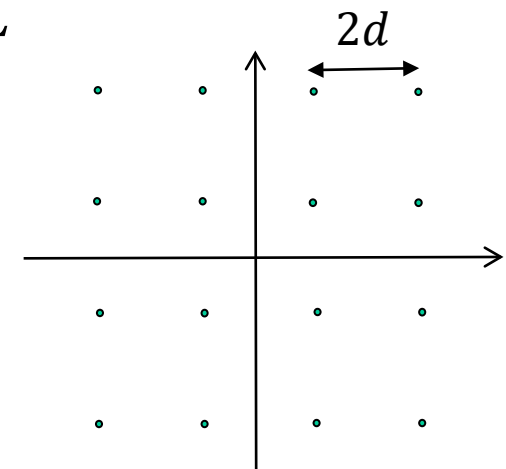
$$d_{\min} = 2d$$

$$E_{s_i} = \int_0^{T_s} s_i^2(t) dt = A_i^2$$

- Average power of a square signal constellation with l bits/dim, P_l

- To increase 1 bit/dim (2 bits/symbol) while maintaining the same $d_{\min}$, the power is needed 4 times as

$$P_{l+1} \approx 4P_l$$



<16QAM>

($M = 16, K = 4,$
 $l = 2, L = 4$)

l : bits per dimension

L^2 : size of constellation

Differential Modulation

- MPSK and MQAM needs carrier phase recovery
→ coherent detection (high complexity and large cost)
- Differential modulation uses the previous symbol as a phase reference for the current symbol (differential phase)
→ DMPSK or DPSK (DBPSK, DQPSK, etc.)
- DPSK Modulation

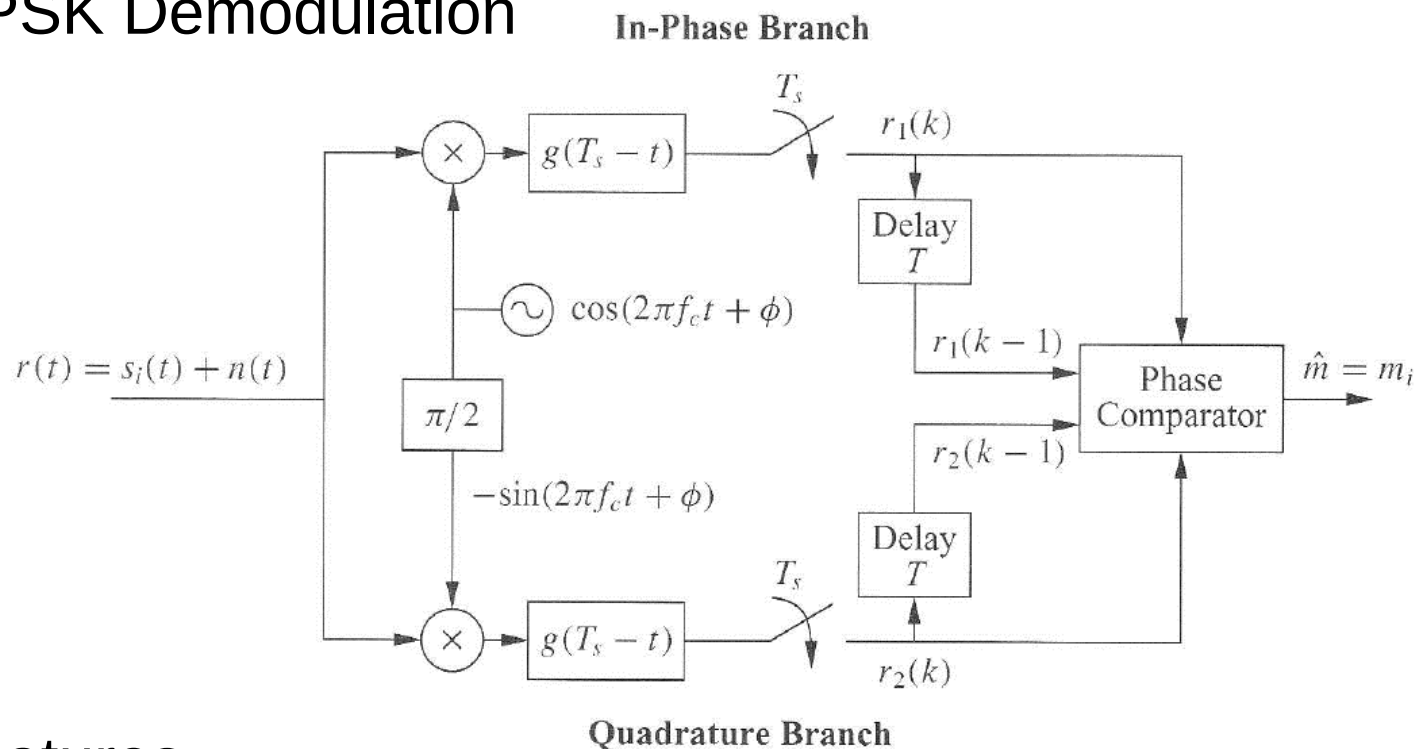
$$\mathbf{r}(k) = Ae^{j(\theta(k)+\varphi_0)} + n(k) \quad n(k): \text{complex WGN}$$

$$\mathbf{r}(k-1) = Ae^{j(\theta(k-1)+\varphi_0)} + n(k-1)$$

$$\begin{aligned} \mathbf{r}(k)\mathbf{r}^*(k-1) = & \boxed{A^2 e^{j(\theta(k)-\theta(k-1))}} + Ae^{j(\theta(k)+\varphi_0)}n^*(k-1) \\ & + Ae^{-j(\theta(k-1)+\varphi_0)}n(k) + n(k)n^*(k-1) \end{aligned}$$

Differential Modulation

■ DPSK Demodulation



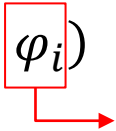
■ Features

- Less sensitive to a random drift in the carrier phase
- Degraded with non-zero Doppler frequency

Frequency Modulation

- Transmit signal over one symbol period

$$s_i(t) = A \cos(2\pi f_i t + \varphi_i)$$

 Phase associated with the i -th carrier

$$s_i(t) = \sum_{j=1}^N s_{ij} \phi_j(t) \quad \text{where} \quad s_{ij} = A\delta(i-j)$$

$\phi_j(t) = \cos(2\pi f_j t + \varphi_j)$ basis functions

- Features

- Constant envelope $\rightarrow$ nonlinear amplifiers can be used
- Robust against amplitude distortion (due to fading or hardware)
- Low spectral efficiency

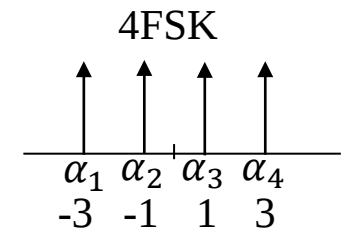
Frequency Shift Keying (FSK)

■ Modulated signal

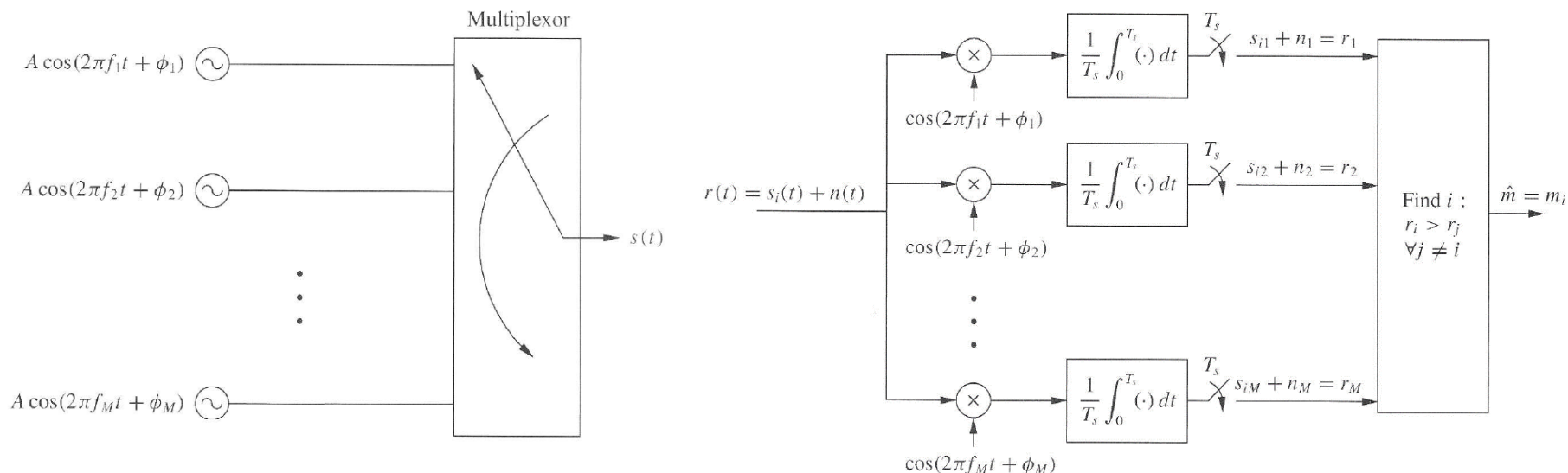
$$s_i(t) = A \cos(2\pi f_c t + 2\pi \alpha_i \Delta f_c t + \varphi_i), \quad 0 \leq t < T_s$$

$$\text{where } \alpha_i = (2i - 1 - M) \text{ for } i = 1, \dots, M = 2^K$$

$$\varphi_i(t) = \sqrt{2/T_s} \cos(2\pi f_c t + 2\pi \alpha_i \Delta f_c t + \varphi_i), \quad i = 1, \dots, M$$

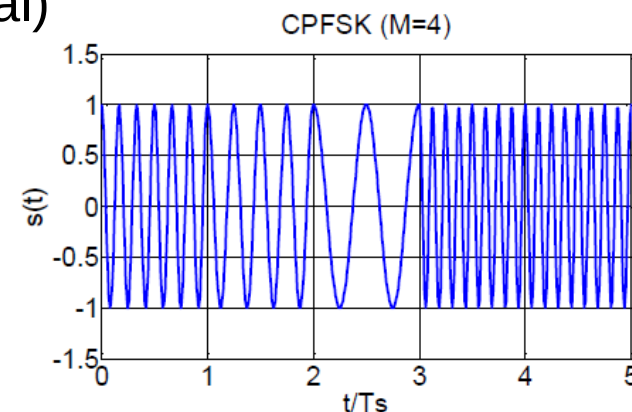


■ Modulator/demodulator (coherent)

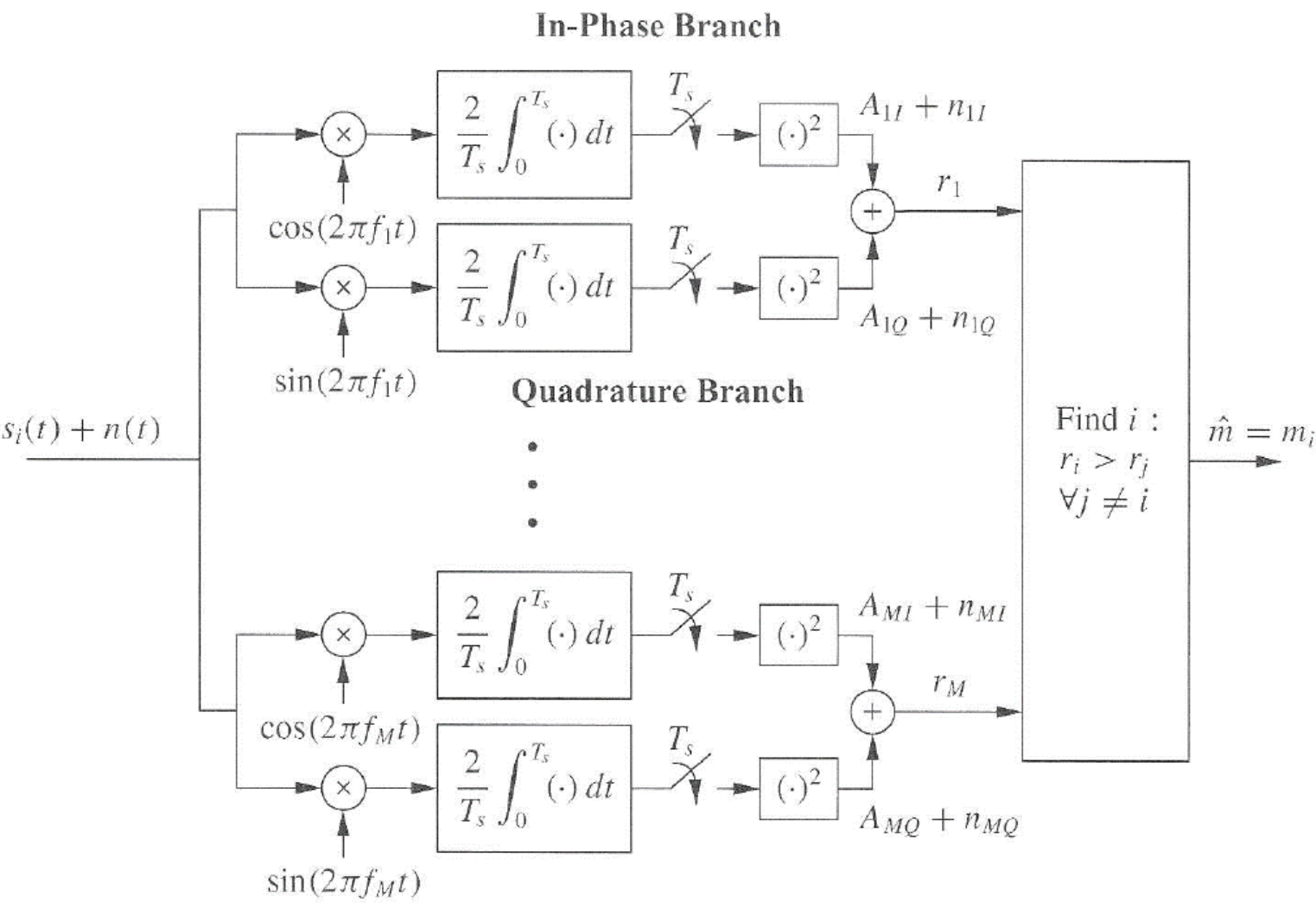


MSK and CPFSK

- MSK (minimum frequency shift keying)
 - Special case of binary FSK when $\varphi_i = \varphi_j$
 - $\Delta f = 2\Delta f_c = 0.5/T_s \rightarrow$ minimum frequency separation for $\langle s_i(t), s_j(t) \rangle = 0$ for $i \neq j$
 - Minimum bandwidth
- CPFSK (Continuous-phase FSK)
 - Phase discontinuity $\rightarrow$ spectrum broadened
 - $s_i(t) = A \cos \left[2\pi f_c t + 2\pi \Delta f_c \int_{-\infty}^t u(\tau) d\tau \right] = A \cos(2\pi f_c t + \theta(t))$
where $u(\tau) = \sum_k a_k g(t - kT)$ (MPAM signal)
 - $\theta(t)$ is continuous
 - Coherent detection in symbol-by-symbol or over a sequence of symbols is available



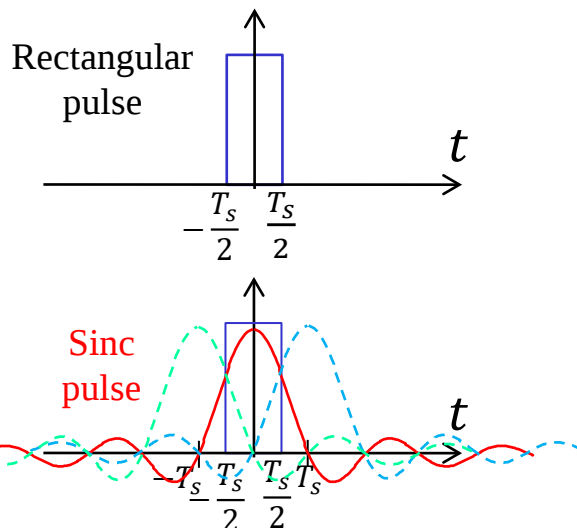
Noncoherent Detection for FSK



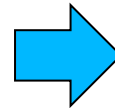
Pulse Shaping

- For amplitude and phase modulation, the signal bandwidth is determined by that of pulse shape $g(t)$
- Pulse shaping
 - Reduce the sidelobe energy (frequency domain property)
 - ISI (inter-symbol-interference) between pulses should be avoided (time domain property)

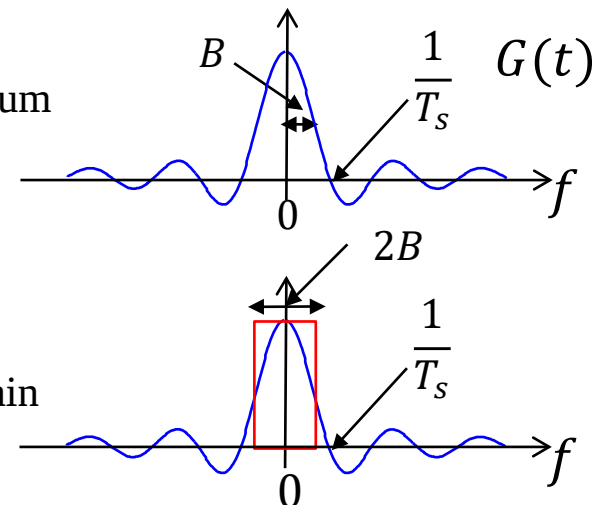
Time domain



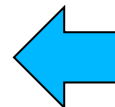
Rectangular pulse
has a broadband spectrum



Frequency domain

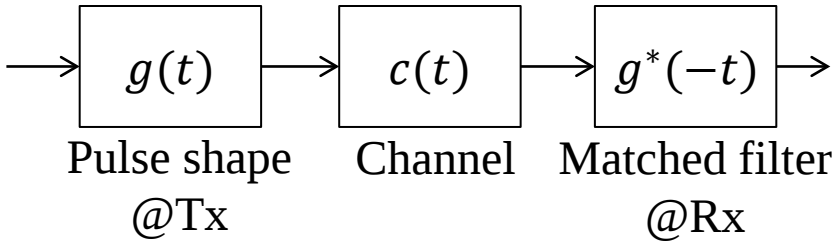


Band-limit signal
is spread in time domain



Optimum Filter Design

- Optimum TRx filter (pulse shaping) design → matched filter

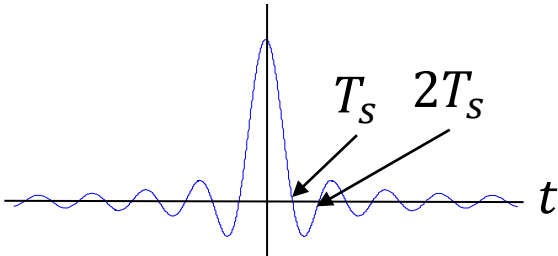


$$p(t) = g(t) * c(t) * g^*(-t)$$
$$= g(t) * g^*(-t)$$

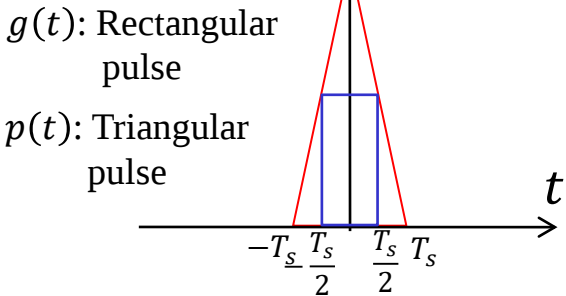
when $c(t) = \delta(t)$ (AWGN)

Nyquist Criterion

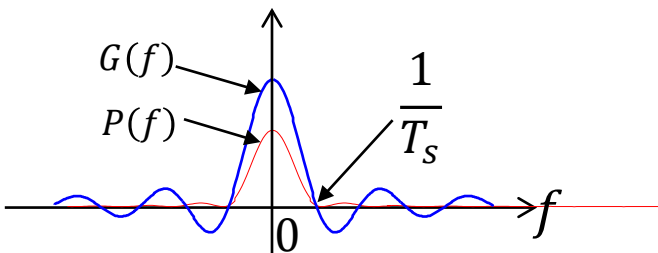
$$p(kT_s) = \begin{cases} p_0 = p(0) & k = 0 \\ 0 & k \neq 0 \end{cases}$$



Time domain



Frequency domain

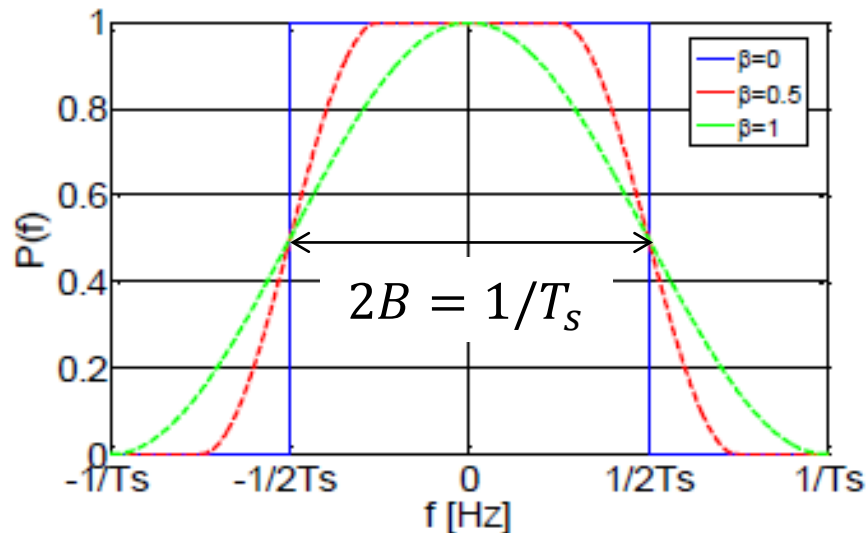


Raised Cosine Pulse

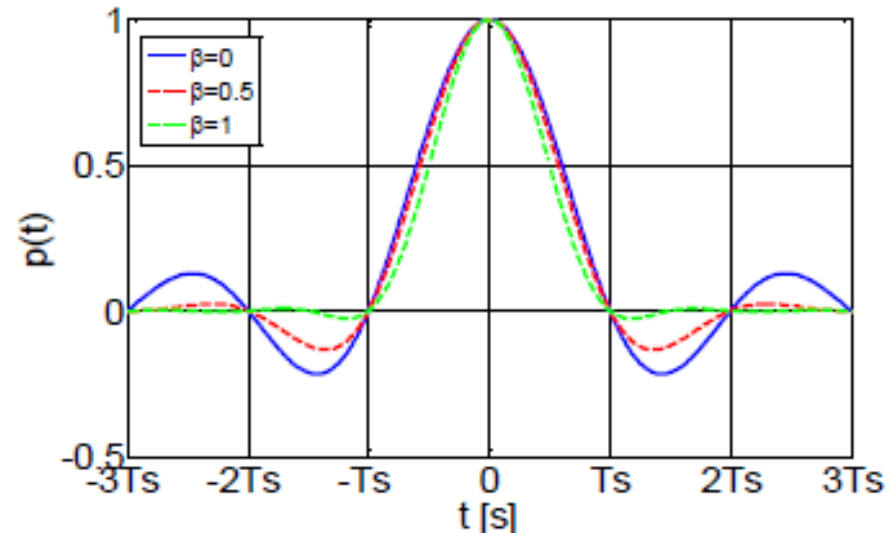
- Most commonly used
- Designed in frequency domain introducing roll-off β

$$P(f) = \begin{cases} T_s & 0 \leq |f| \leq \frac{1-\beta}{2T_s} \\ \frac{T_s}{2} \left[1 - \sin \frac{\pi T_s}{\beta} \left(f - \frac{1}{2T_s} \right) \right] & \frac{1-\beta}{2T_s} \leq |f| \leq \frac{1+\beta}{2T_s} \end{cases}$$

$$p(t) = \frac{\sin \pi t / T_s}{\pi t / T_s} \frac{\cos \beta \pi t / T_s}{1 - 4\beta^2 t^2 / T_s^2}$$



frequency domain



Time domain

Outline

- Performance Criteria
 - Probability of error
 - Outage probability

- Error sources
 - Noise
 - Flat fading
 - Frequency selective fading → ISI (Inter symbol interference)
 - Time selective fading (Doppler) → ACI (Adjacent channel interference)

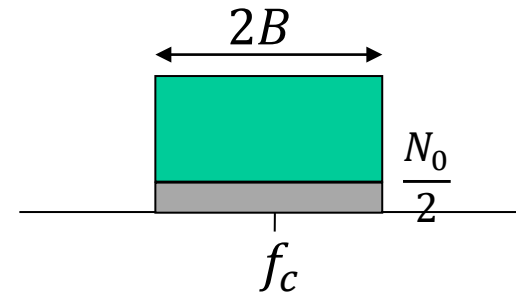
Signal to Noise Power Ratio (SNR)

- Signal to noise power ratio (SNR)

$$\text{SNR} = \frac{P_r}{N_0 B} = \frac{E_s}{N_0 B T_s}$$

$$\gamma_s = \frac{E_s}{N_0}$$

$$\gamma_b = \frac{E_b}{N_0}$$



For general pulses, $T_s = k/B$

$k = 1$ for pulse shaping with $\beta = 1$

$k = 0.5$ for rectangular pulse

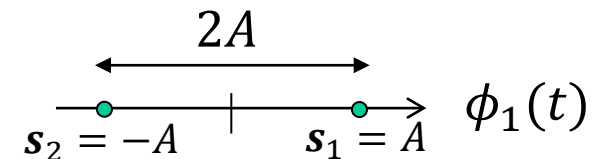
For M-ary signaling (MPAM and MPSK), $\gamma_b = \frac{\gamma_s}{\log_2 M}$

Error Probability in AWGN Channel

■ Error probability for BPSK

$$P_s \approx M_{\text{dmin}} Q\left(\frac{d_{\text{min}}}{\sqrt{2N_0}}\right) = Q\left(\sqrt{\frac{2A^2}{N_0}}\right) = Q\left(\sqrt{\frac{2E_b}{N_0}}\right)$$

$$P_b = P_s = Q(\sqrt{2\gamma_b})$$

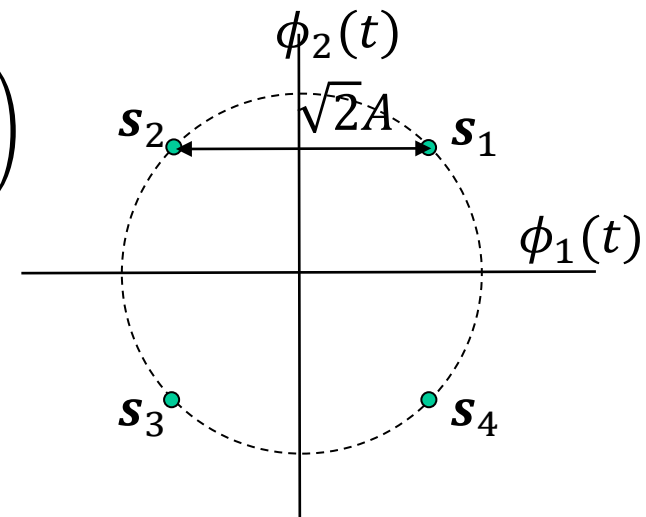


■ Error probability for QPSK

$$P_s \approx M_{\text{dmin}} Q\left(\frac{d_{\text{min}}}{\sqrt{2N_0}}\right) = 2Q\left(\frac{\sqrt{2A^2}}{\sqrt{2N_0}}\right) = 2Q\left(\sqrt{\frac{A^2}{N_0}}\right)$$

$$= 2Q(\sqrt{\gamma_s})$$

$$P_b = Q(\sqrt{2\gamma_b}) \text{ for gray code}$$



Error Probability in AWGN Channel

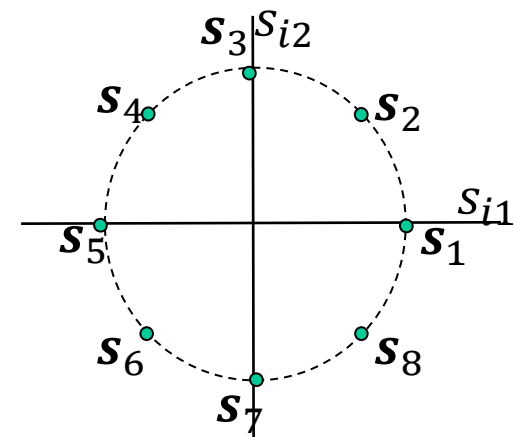
■ Error probability for MPSK

$$P_s \approx M_{d_{\min}} Q \left(\frac{d_{\min}}{\sqrt{2N_0}} \right) = 2Q \left(\sqrt{2} \sin \frac{\pi}{M} \sqrt{\frac{A^2}{N_0}} \right) = 2Q \left(\sqrt{2\gamma_s} \sin \frac{\pi}{M} \right)$$

$$P_b = \frac{2}{\log_2 M} Q \left(2\sqrt{2 \log_2 M \gamma_b} \sin \frac{\pi}{M} \right)$$

$$s_{i1}(t) = A \cos \left(2\pi \frac{(i-1)}{M} \right),$$

$$s_{i2}(t) = A \sin \left(2\pi \frac{(i-1)}{M} \right)$$



<8PSK($M = 8, K = 3$)>

Error Probability in AWGN Channel

■ Error probability for MPAM

$$P_s = \frac{1}{M} \sum_{i=1}^M P_s(\mathbf{s}_i)$$

$$P_s \approx \frac{M-2}{M} 2Q\left(\frac{2d}{\sqrt{2N_0}}\right) + \frac{2}{M} Q\left(\frac{2d}{\sqrt{2N_0}}\right)$$

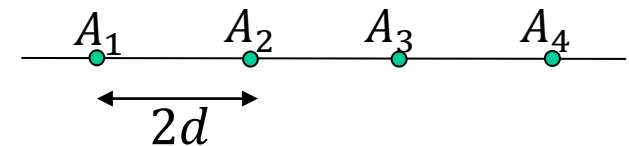
$$= 2\left(\frac{M-1}{M}\right) Q\left(\sqrt{\frac{2d^2}{N_0}}\right) = 2\left(\frac{M-1}{M}\right) Q\left(\sqrt{\frac{1}{N_0} \frac{6\bar{E}_s}{M^2-1}}\right)$$

$$= 2\left(\frac{M-1}{M}\right) Q\left(\sqrt{\frac{6\bar{\gamma}_s}{M^2-1}}\right)$$

$$\text{where } \bar{E}_s = \frac{1}{M} \sum_{i=1}^M A_i^2 = \frac{d^2}{M} \sum_{i=1}^M (2i-1-M)^2 = \frac{1}{3} (M^2-1)d^2$$

$$P_b = \frac{2}{\log_2 M} \left(\frac{M-1}{M}\right) Q\left(\sqrt{\frac{6\bar{\gamma}_b \log_2 M}{M^2-1}}\right)$$

$$A_i = (2i-1-M)d, \quad i = 1, \dots, M$$



<4PAM($M = 4, K = 2$)>

Differential Modulation

■ DPSK

$$\mathbf{r}(k) = Ae^{j(\theta(k)+\varphi_0)} + n(k)$$

$n(k)$: complex WGN

$$\mathbf{r}(k-1) = Ae^{j(\theta(k-1)+\varphi_0)} + n(k-1)$$

$$\begin{aligned} \mathbf{z} = \mathbf{r}(k)\mathbf{r}^*(k-1) &= \boxed{A^2 e^{j(\theta(k)-\theta(k-1))}} \\ &\quad + \underbrace{Ae^{j(\theta(k)+\varphi_0)}n^*(k-1) + Ae^{-j(\theta(k-1)+\varphi_0)}n(k)}_{\text{Noise increases twice}} \\ &\quad + \underbrace{n(k)n^*(k-1)}_{\text{very small negligible}} \end{aligned}$$

■ Error Probability

$$P_b = \frac{1}{2} e^{-\gamma_b} \quad (\text{DBPSK})$$

$$P_b = \int_b^\infty x \exp\left[-\frac{(a^2 + x^2)}{2}\right] I_0(ax) dx - \frac{1}{2} \int_b^\infty x \exp\left[-\frac{(a^2 + b^2)}{2}\right] I_0(ab) dx \quad (\text{DQPSK})$$

where $a \approx 0.765\sqrt{\gamma_b}$, $b \approx 1.85\sqrt{\gamma_b}$

Error Probability in AWGN (Summary)

- Coherent detection: perfect carrier phase recovery

Modulation	$P_s(\gamma_s)$	$P_b(\gamma_b)$
BFSK:		$P_b = Q(\sqrt{\gamma_b})$
BPSK:		$P_b = Q(\sqrt{2\gamma_b})$
QPSK, 4QAM:	$P_s \approx 2 Q(\sqrt{\gamma_s})$	$P_b \approx Q(\sqrt{2\gamma_b})$
MPAM:	$P_s \approx \frac{2(M-1)}{M} Q\left(\sqrt{\frac{6\gamma_s}{M^2-1}}\right)$	$P_b \approx \frac{2(M-1)}{M \log_2 M} Q\left(\sqrt{\frac{6\gamma_b \log_2 M}{(M^2-1)}}\right)$
MPSK:	$P_s \approx 2Q(\sqrt{2\gamma_s} \sin(\pi/M))$	$P_b \approx \frac{2}{\log_2 M} Q(\sqrt{2\gamma_b \log_2 M} \sin(\pi/M))$
Rectangular MQAM:	$P_s \approx \frac{4(\sqrt{M}-1)}{\sqrt{M}} Q\left(\sqrt{\frac{3\gamma_s}{M-1}}\right)$	$P_b \approx \frac{4(\sqrt{M}-1)}{\sqrt{M} \log_2 M} Q\left(\sqrt{\frac{3\gamma_b \log_2 M}{(M-1)}}\right)$
Nonrectangular MQAM:	$P_s \approx 4Q\left(\sqrt{\frac{3\gamma_s}{M-1}}\right)$	$P_b \approx \frac{4}{\log_2 M} Q\left(\sqrt{\frac{3\gamma_b \log_2 M}{(M-1)}}\right)$

Table 6.1: Approximate Symbol and Bit Error Probabilities for Coherent Modulations

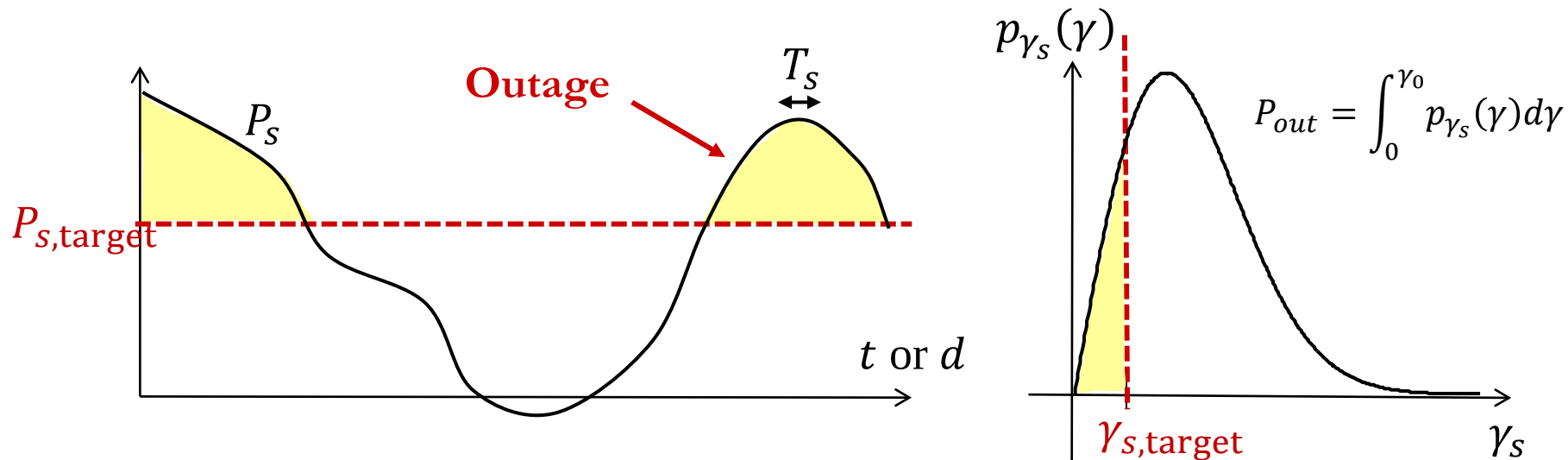
$$P_s \approx \alpha_M Q(\sqrt{\beta_M \gamma_s})$$

$$P_b \approx \frac{\alpha_M}{\log_2 M} Q(\sqrt{\beta_M \gamma_b \log_2 M})$$

Fading Channel

- Received signal power varies randomly over distance or time as a result of shadowing and multipath fading
 - γ_s is a random variable with $p_{\gamma_s}(\gamma)$, and so $P_s(\gamma_s)$ is also random
- Performance criteria
 - Outage probability $P_{\text{out}} = \Pr(P_s > P_{\text{target}}) = \Pr(\gamma_s < \gamma_{\text{target}})$
 - Average error probability $\bar{P}_s = \int_0^\infty P_s(\gamma) p_{\gamma_s}(\gamma) d\gamma$
 - Combined average error probability and outage probability

Outage Probability

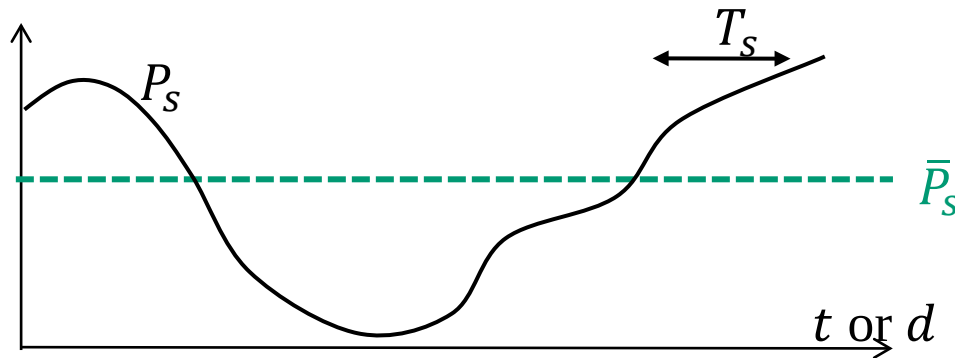


- Probability that P_s is above target
- Equivalently, probability γ_s below target
- Used when $T_c \gg T_s$

$$P_{out} = \Pr(P_s > P_{target})$$

$$= \Pr(\gamma_s < \gamma_{target})$$

Average P_s



$$\bar{P}_s = \int_0^{\infty} P_s(\gamma) p_{\gamma_s}(\gamma) d\gamma$$

- Expected value of random variable P_s
- Used when $T_c \approx T_s$
- Error probability much higher than in AWGN alone

Average P_s

- Rayleigh fading

$$p_r(r) = \frac{r}{\sigma^2} \exp\left[-\frac{r^2}{2\sigma^2}\right] \quad \gamma = \frac{r^2 T_s}{2\sigma_n^2}$$

$$p_{\gamma_s}(\gamma) = \frac{\sigma_n^2}{\sigma^2 T_s} \exp\left[-\frac{\gamma \sigma_n^2}{\sigma^2 T_s}\right] = \frac{1}{\bar{\gamma}_s} \exp\left[-\frac{\gamma}{\bar{\gamma}_s}\right]$$

- Example average BER

$$\bar{P}_b = \int_0^\infty P_b(\gamma) p_{\gamma_b}(\gamma) d\gamma$$

- BPSK: $P_b(\gamma) = Q(\sqrt{2\gamma_b})$, $\bar{P}_b = \frac{1}{2} \left[1 - \sqrt{\frac{\bar{\gamma}_b}{1+\bar{\gamma}_b}} \right] \approx \frac{1}{4\bar{\gamma}_b}$

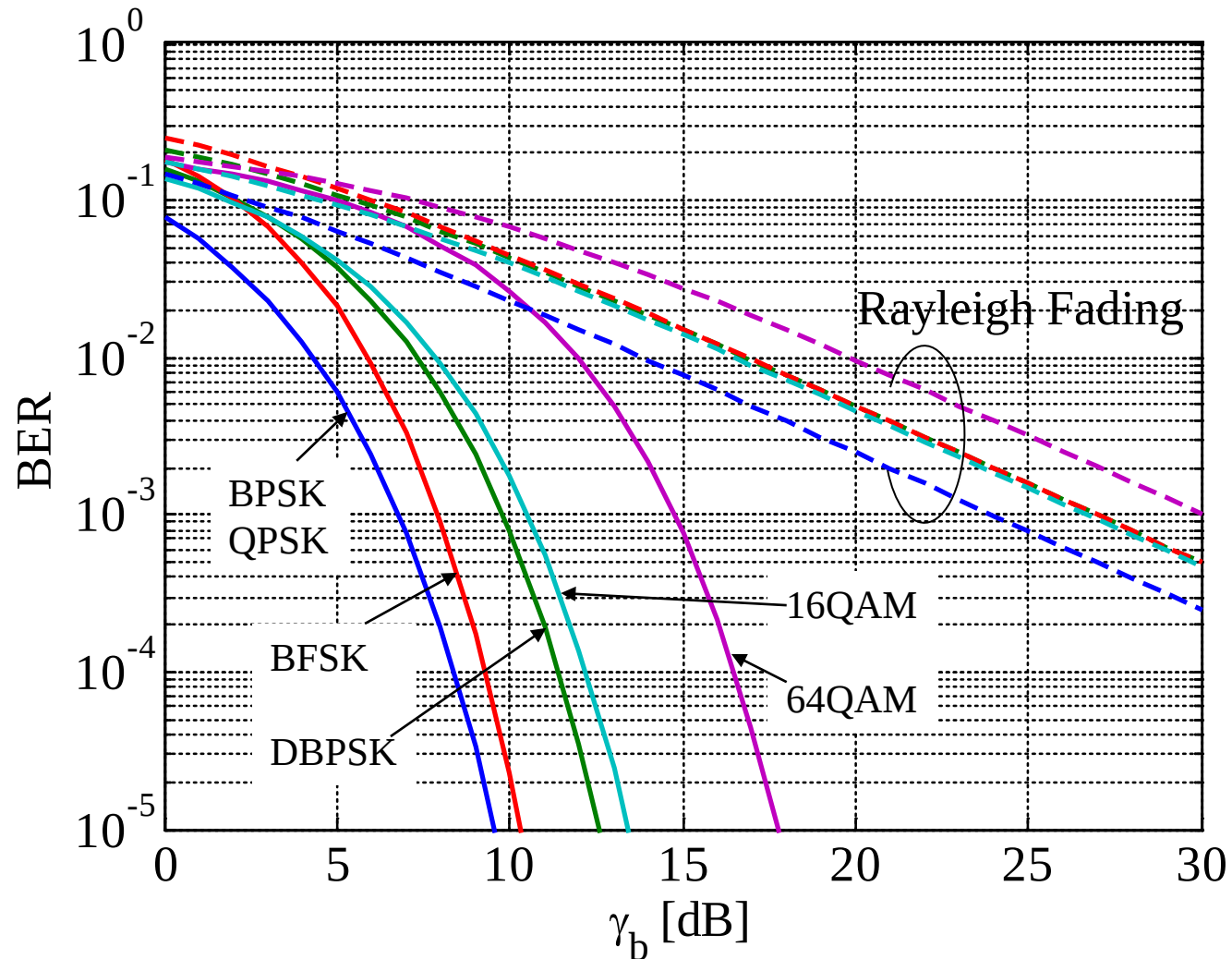
- BFSK: $P_b(\gamma) = Q(\sqrt{\gamma_b})$, $\bar{P}_b = \frac{1}{2} \left[1 - \sqrt{\frac{\bar{\gamma}_b}{2+\bar{\gamma}_b}} \right] \approx \frac{1}{4\bar{\gamma}_b}$

- DBPSK: $P_b(\gamma) = \frac{1}{2} e^{-\gamma_b}$, $\bar{P}_b = \frac{1}{2(1+\bar{\gamma}_b)} \approx \frac{1}{2\bar{\gamma}_b}$

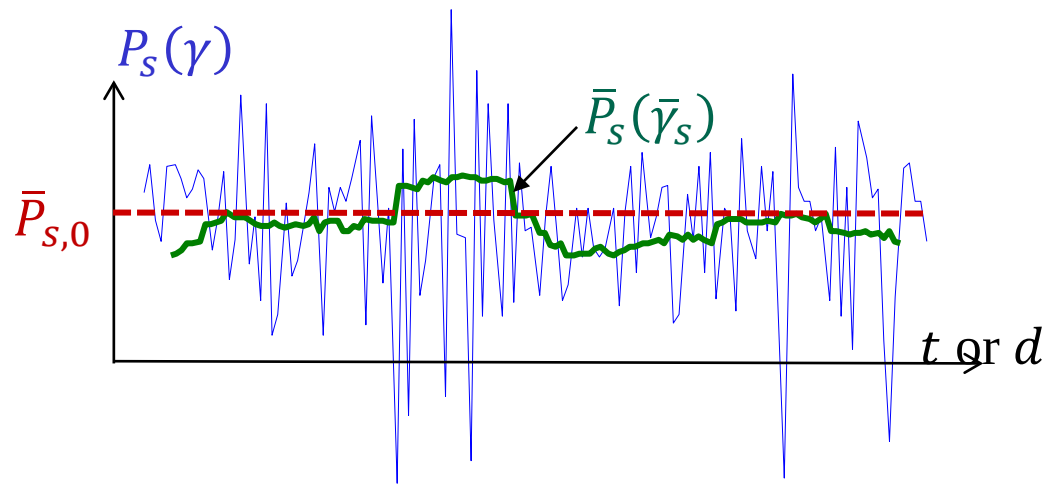
- General: $P_s(\gamma) \approx \alpha_M Q(\sqrt{\beta_M \gamma_s})$, $\bar{P}_s = \frac{\alpha_M}{2} \left[1 - \sqrt{\frac{0.5\beta_M \bar{\gamma}_b}{1+0.5\beta_M \bar{\gamma}_b}} \right] \approx \frac{\alpha_M}{2\beta_M \bar{\gamma}_b}$

Average P_s

■ AWGN vs Rayleigh fading



Combined Outage and Average P_s



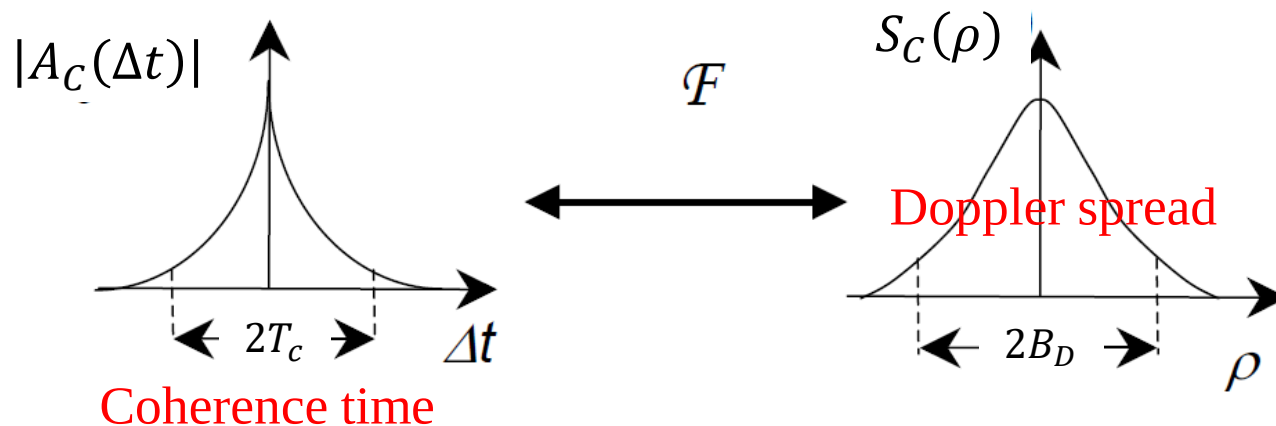
$$\bar{P}_s(\bar{\gamma}_s) = \int_0^\infty P_s(\gamma_s) p(\gamma_s | \bar{\gamma}_s) d\gamma_s$$

$$\bar{P}_{s0} = \int_0^\infty P_s(\gamma_s) p(\gamma_s | \bar{\gamma}_{s0}) d\gamma_s$$

- When fading environment is superposition of both fast and slow fading
 - Used in combined **shadowing** and **flat-fading**
- $\bar{P}_s$ varies slowly, locally determined by flat fading
- Declare outage when $\bar{P}_s$ above target value

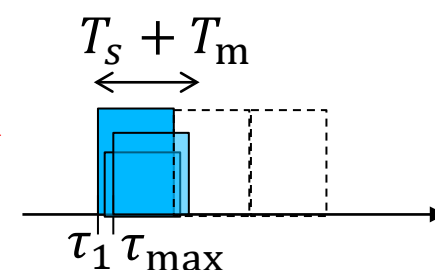
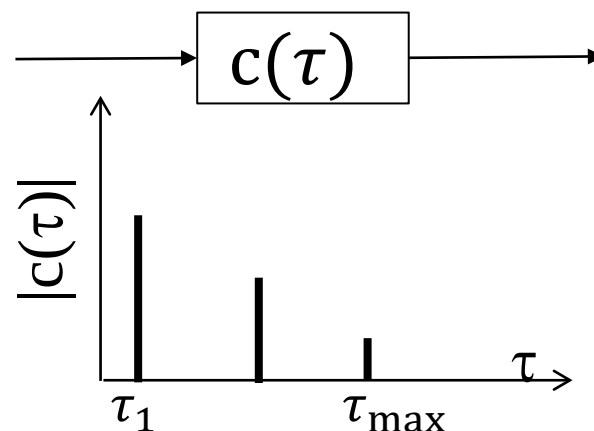
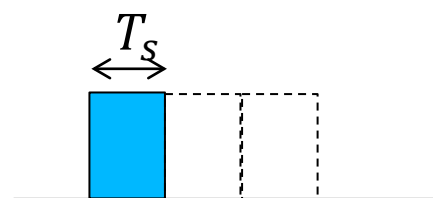
Doppler Effect

- High Doppler causes channel phase to decorrelate between symbols
- Leads to an irreducible error floor for differential modulation
- Increasing power does not reduce error
- Error floor depends on $B_D T_S$

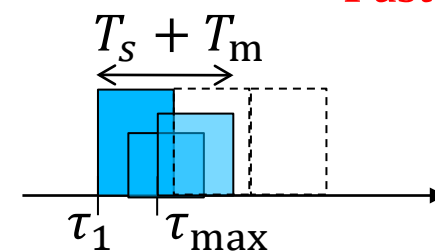


Inter-Symbol Interference

- Delay spread exceeding a symbol time causes ISI (self interference) → frequency selective fading
- ISI leads to irreducible error floor
 - Increasing signal power increases ISI power
- ISI requires that $T_s \gg \sigma_{\tau_m}$ ($R_s \ll B_c$)



Non resolvable → Fast fading



Resolvable → ISI